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Poly(ethylene oxide) bionanocomposites reinforced with chitin nanofiber networks



^a School of Materials Science and Engineering, Georgia Institute of Technology, Atlanta, GA 30332, USA

^b School of Chemical and Biomolecular Engineering, Georgia Institute of Technology, Atlanta, GA 30332, USA

^c Renewable Bioproducts Institute, Georgia Institute of Technology, Atlanta, GA 30332, USA

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ABSTRACT

With excellent reinforcing performance and many remarkable inherent properties, such as renewability and high strength-per-unit-mass, chitin nanofibers (ChNFs) are attractive resources for polymer composite applications. However, significant challenges resulting from chitin's insolubility have hindered efforts to incorporate it effectively into polymer matrices. Here, ChNFs extracted from crab shells were used as fillers to reinforce polyethylene oxide (PEO). The dispersion of ChNFs in the polymer matrix and the interactions between fiber and matrix were studied by utilizing solvent-etching of the polymer matrix, FTIR spectroscopy and AFM colloidal probe adhesion measurements. The results show that the ChNFs were dispersed well and formed a fine interconnected network structure in the PEO matrix. ChNFs also exhibited strong adhesion with PEO, resulting from hydrogen bond and van der Waals forces. The ChNF interconnected network greatly enhanced the mechanical properties of PEO, with a 3-fold increase in both the tensile strength and elastic modulus of the nanocomposites at 20% ChNF loading. Processing ChNFs in suspensions with slight acidity and water-soluble polymers appears to support the formation of highly interconnected networks that makes ChNF-polymer composites excellent candidates for reinforced, light-weight, renewable materials.

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1. Introduction

The development of nanofiller-reinforced polymer composites has attracted intense attention from researchers over the past two decades due to the large surface area/volume ratio of nanofillers, and various materials have been utilized to enhance the mechanical properties of polymer matrices, such as single-walled/multi-walled carbon nanotubes, layered silicate and nanocellulose [1–7]. To date, tremendous efforts have been devoted to improving filler adhesion with polymers and their dispersion in matrices since these two factors significantly influence stress transfer in nanocomposites. Methods applied to address these issues include physicalmechanical treatment and chemical functionalization [2–7]. However, it is still challenging to enhance particle or fiber dispersion and adhesion with the matrix simultaneously [2–7].

E-mail address: carson.meredith@chbe.gatech.edu (J.C. Meredith).

¹ These authors contributed equally.

Chitin, the second most abundant naturally occurring polymer. forms a highly ordered crystalline structure in living organisms [8,9]. Nanosized crystalline chitin (chitin nanocrystal or chitin nanowhisker) can be produced by strong acid hydrolysis, and shows excellent mechanical properties, such as a longitudinal modulus of 150 GPa and transverse modulus of 15 GPa [10]. Recently, our group reported that ChNFs with diameter of ~20 nm could be extracted from crab shells by a high pressure homogenization process [11,12]. The size and mechanical properties of ChNF features make them ideal reinforcing materials for polymer matrices. PEO is a water-soluble and biocompatible semicrystalline polymer that has found applications in many fields, such as electrolytes, and biomedical engineering [1,13,14]. However, its low modulus and tensile strength limit applications. These mechanical limitations and its water solubility make PEO an ideal model system for examining dispersion, adhesion and strengthening possible with ChNFs. In this work, we prepared ChNF-PEO composites with up to 20% ChNF content. Solvent-etching of the polymer matrix followed by SEM, FTIR spectroscopy and AFM colloidal probe adhesion measurements were used to study the ChNF dispersion and adhesion between ChNF and PEO matrix. The





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^{*} Corresponding author. School of Chemical and Biomolecular Engineering, Georgia Institute of Technology, Atlanta, GA, 30332, USA.

results demonstrate that without utilizing chemical surface modification, ChNFs can be readily dispersed in PEO, form a remarkable interconnected network nanostructure and have strong adhesion with PEO, significantly enhancing tensile strength and elastic modulus simultaneously.

2. Experimental section

2.1. Materials

Dried crab shell flakes were purchased from TCI America. Deionized water (18.2 M Ω cm) was prepared in a Barnstead Easypure RoDi purification system. Hydrochloric acid, sodium hydroxide, acetone and ethanol were purchased from EMD Chemical Inc. Poly(ethylene oxide) (PEO, Mv = 1,000,000 g/mol, Sigma–Aldrich), poly(ethylene) (PE, Mw = 40,000 g/mol, Sigma–Aldrich), poly(styrene) (PS, Mw = 230,000 g/mol, Sigma–Aldrich), poly(styrene) (PS, Mw = 50,000 g/mol, Alfa Aesar), and poly(vinyl alcohol) (PVOH, Mw = 89,000-98,000 g/mol, Sigma–Aldrich) were used as received without further purification. 1, 2, 3trichlorobenzene (TCB, Sigma–Aldrich), hexafluoroisopropanol (HFIP, TCI America), and toluene (Sigma–Aldrich), glycerol (Alfa Aesar, purity> 99%) and diiodomethane (Alfa Aesar, purity>99%) were used as received. Polystyrene (PS) particle with diameters of ~10 µm was purchased from Alfa Aesar Inc.

2.2. Methods

2.2.1. Preparation of ChNFs

Dried crab shell flakes were processed to obtain purified chitin [11,12,15,16]. Ground crab shells were refluxed in 5 wt % sodium hydroxide in DI water for 6 h to remove protein. The suspension was filtered and rinsed with DI water until the pH was 7. Next, the filtered solids were treated with 7% hydrochloric acid for 6 h at room temperature to remove minerals. After filtration and washing with DI water, the treated sample was refluxed in a 5% NaOH solution for 2 days to remove residual proteins. A final extraction with acetone and ethanol was used to remove any remaining residues (soluble dye for example). The purified chitin was dispersed in distilled water under acidic condition and then this mixture was passed through a high-pressure homogenizer (Bee International Inc., MA) to generate ChNFs (aqueous medium pH is ~4.1). Detailed information on ChNF production is described elsewhere [11].

2.2.2. Preparation of ChNF/PEO nanocomposite films

The PEO was firstly dissolved at 2 wt.% in DI water at room temperature under a magnetic stirring. To prepare 5, 10, 15 and 20 wt.% ChNF/PEO composite films, the proper amount of ChNF/ water dispersions were added to the PEO solution. These mixtures were magnetically stirred for two days, and were subsequently casted into a PS Petri dish, followed by drying under vacuum at 40 °C for two days. The free standing dried ChNF/PEO nano-composite films were obtained by carefully peeling films from the PS substrate. Neat PEO films were prepared using the same processing conditions for comparison. Both neat PEO and composite films had a thickness of ~50 μ m, as determined by an interferometer (Model ID-C112CEB, Mitutoyo Corp.).

2.2.3. Preparation of ChNF coated polystyrene (PS) colloidal particles

In order to fabricate colloidal probes coated with ChNFs for adhesion measurements, a 0.5 wt. % ChNF in water dispersion was added to a PS particle suspension (10 μ m, 2.5 wt % in water),

followed by agitation using a rotational shaker for 12 h. The mixture was then centrifuged in a micro-centrifuge (VWR Micro 1207). The ChNF coated PS particles were settled at the bottom of the container and dried in air at room temperature.

2.2.4. Preparation of polymer films

Substrates for colloidal-probe adhesion studies were prepared by coating a series of polymer films on Piranha-cleaned silicon wafers. The PE solution was prepared by dissolving 5% PE by mass in hot 1, 2, 3-trichlorobenzene at ~100 °C. The PS solution was prepared by dissolving 10% PS by mass in toluene. 5 wt. % PVOH and PVAc solutions were prepared in hexafluoroisopropanol. The PEO solution was prepared by dissolving 1 wt. % by mass in DI water. Polymer films were prepared on Piranha-etched silicon substrates, by using a knife-edge coating method described in detail elsewhere [17]. The cast polymer films were firstly dried at room temperature for 24 h and then dried under vacuum for at least 12 h (PVAc at 20 °C for 48 h and other polymers at 60 °C for 12 h) to remove the residual solvent. After drying, films were transferred to a desiccator and stored prior to measurements. Film thickness was approximately 10–20 µm, determined by using an interferometer (Model ID-C112CEB, Mitutoyo Corp.).

2.2.5. Measurements of adhesion forces

Adhesion force measurements were carried out using atomic force microscopy (AFM) (Veeco Dimension 3100). Tipless rectangular cantilevers with nominal spring constants of 0.6-3.7 N/m (Applied NanoStructures, Inc., Santa Clara, CA) were used. Single ChNF-coated or bare PS particles were glued to the tipless cantilevers with a small amount of epoxy resin (Epoxy Marine, Loctite, Westlake, OH USA) using a procedure described in detail elsewhere [18]. The actual spring constants for the cantilevers with the attached ChNF-coated or bare PS particles (0.7-1.1 N/m) were determined directly by the methods of Burnham and Hutter et al. [19]. A series of 20 force-distance curves were measured for each combination of PS/ChNF or bare PS tip-polymer surface, taken on three separate substrate surfaces within three randomly chosen 1 cm \times 1 cm areas on each substrate at 20 °C, humidity 25–30%. Three separate ChNF-coated or bare PS particle tips were used for each set of measurements with a given substrate. The applied load during force measurements was 2.5 nN. The mean (R_a) and rootmean-square (rms) surface roughness of each polymer film for adhesion measurements were obtained from topography scans of three randomly-chosen 10 μ m \times 10 μ m areas on each polymer surface by using AFM with a standard pyramidal silicon nitride probe.

2.2.6. Contact angle measurements

Contact angles of each polymer surface were measured at 20 °C using a video contact angle system (AST products 2500XE, Billerica, MA). Three standard testing liquids were chosen, two polar liquids (DI-water and glycerol) and one nonpolar (diiodomethane), to calculate the surface tension components of each polymer surfaces. The water contact angles of those polymer surfaces were measured only 3-5 s after drop placement. Generally, we didn't observe a significant change of the contact angle until after at least 15 s, which presumably occurs due to dissolution of the substrate. Nine 1 μ L drops of each liquid were used for the contact angle test of each polymer surface. Surface tension components corresponding to van der Waals (VDW), Lewis acid, and Lewis basic interactions were calculated from measured contact angle data by using van Oss and Good's van der Waals acid-base theory [20]. According to this theory, the surface energy is accessed from Eq. (1).

$$\gamma_S = \gamma_S^{\nu W} + 2\left(\gamma_S^+ \gamma_S^-\right)^{1/2} \tag{1}$$

where, γ_S is the total surface tension, $\gamma_S^{\nu W}$ is the van der Waals component, γ_S^+ is the acid (electron acceptor) component, and γ_S^- is the base (electron donor) component of the solid substrate. The relation between surface energy components and the liquid-solidair contact angle (θ) is given as:

$$\gamma_L(1+\cos\theta) = 2\left(\gamma_S^{\nu W}\gamma_L^{\nu W}\right)^{1/2} + 2\left(\gamma_S^+\gamma_L^-\right)^{1/2} + 2\left(\gamma_L^+\gamma_S^-\right)^{1/2}$$
(2)

where, γ_L represents the surface energy of the testing liquids. By using the known components of γ_L for three carefully-chosen liquids, the γ_S components can be determined by regression. The surface tensions of the testing liquids are as follows: water, $\gamma^+ = \gamma^- = 25.5$, $\gamma^{vW} = 21.8$, $\gamma = 72.8$ mJ/m²; glycerol, $\gamma^+ = 3.92$, $\gamma^- = 57.4$, $\gamma^{vW} = 34.0$, $\gamma = 64.0$ mJ/m²; diiodomethane, $\gamma^+ = \gamma^- = 0$, $\gamma^{vW} = 50.8$, $\gamma = 50.8$ mJ/m² [21,22].

2.2.7. Characterizations of ChNFs

The morphologies of the prepared materials were characterized using Field-Emission Scanning Electron Microscopy (SEM, Zeiss Ultra 60, Carl Zeiss SMT, Ltd., Thornwood, NY). Before imaging, these samples were coated with a thin layer of gold/palladium (Hummer IV Sputtering System) to prevent sample charging. A solvent-etching procedure was used to selectively remove PEO domains from composites in order to aid in visualization of the ChNF morphology. Etched films were prepared by washing with water followed by rinsing with ethanol and drying at room temperature for 2 days prior to SEM imaging.

The attenuated total reflectance-Fourier transform infrared spectra (ATR-FTIR) of ChNF, neat PEO and nanocomposite films were recorded using a Bruker Vertex 80v FTIR spectrometer coupled to a Hyperion 2000 IR microscope under a 20x magnification ATR objective (Bruker Optics, Inc., Billerica, MA). Measurements were collected from 4000 to 400 cm⁻¹ with a resolution of 4 cm⁻¹, and were averaged over 64 scans. The surface charge of ChNFs at pH 4.1 in water was measured by a Malvern Zetasizer Nano ZS 90.

Mechanical characterization of neat PEO and PEO nanocomposites was conducted using a high-throughput mechanical characterization (HTMECH) apparatus under ambient conditions, described in detail elsewhere [23,24]. Briefly, the polymer films were mounted in between two stainless steel plates and indented by a steel pin with a diameter of 1.5 mm at a constant strain rate (0.5 mm/s), resulting in equi-biaxial deformation. For each sample, a minimum of 9 stress-strain tests were performed to obtain films' mechanical properties, such as elastic modulus and tensile strength.

The glass transition temperatures of the materials were measured using dynamic mechanical analysis (DMA, Q800, TA Instruments, DE USA). The samples were cut into rectangular strips about ~3 cm long and ~3 mm wide and were tested in a tension mode while being heated from -90 °C to 40 °C with a heating rate of 2 °C/min at a frequency of 1 Hz. All tests were performed in the linear viscoelastic region.

Differential scanning calorimetry (DSC) (Q200, TA Instruments, USA) was used to obtain the melting temperature and crystallinity of neat PEO and PEO nanocomposites. Approximately 5–10 mg of sample was loaded into aluminum pan. The PEO samples were

heated and cooled at a rate of 10 C/min under a nitrogen flow of 50 mL/min. The samples were firstly cooled from room temperature to -80 °C, held at -80 °C for 5 min, and were heated to 120 °C, followed by maintaining at this temperature for 5 min and cooling to room temperature.

3. Results and discussion

3.1. Morphologies of ChNF/PEO nanocomposite films

ChNFs produced from the high-pressure homogenization process have an average diameter of 20 nm, mainly ranging from 5 to 50 nm and lengths that vary between hundreds of nanometers to several micrometers, as shown in Fig. S1. They have a zeta potential of +57.5 mV at pH 4.1 due to protonated $-NH_3^+$ groups [11]. SEM images of the as-prepared films, shown as cross-section (Fig. 1 A, B, and Fig. S2) and top-view (Fig. 1C, D) indicated that 10% and 20% ChNF composites have void-free surfaces. The outlines of fibrous morphologies assumed to be ChNFs can be observable, suggesting that ChNFs were imbedded in the PEO matrix and had good adhesion with PEO. However, the identity, size and interconnectivity of the ChNFs cannot be observed directly from Fig. 1 A-D. Since PEO is water soluble, but ChNFs are not, a solventetching procedure was used to selectively remove PEO domains in composites. As shown in supplementary data (Fig. S3), neat PEO films were totally dissolved within 3 h of water immersion, while ChNF/PEO composites maintained their shape after 10 days of water immersion and 3 days of ethanol immersion before drying. Fig. 1E and F shows SEM images of the top surfaces of the dried solvent-etched 10% and 20% ChNF composite films, respectively. Porous fibrous network structures are observed in both samples, and most fibers in the 10% ChNF sample (Fig. 1 E) have diameters ranging from 5 to 50 nm. Despite more fiber aggregates being observed for 20% ChNF/PEO, there are still many fibers with diameters of below 50 nm (Fig. 1 F). Fig. 1 and Fig. S3 clearly show that the ChNFs were dispersed well and formed network structures in the PEO matrix. We propose that the good dispersion of ChNFs is ascribed to the excellent dispersion of ChNFs in water before their mixing with PEO, electrostatic repulsion between ChNFs in PEO solution (pH < 6), and strong adhesion between ChNF and PEO, as discussed below in detail.

3.2. Mechanical properties of ChNF/PEO nanocomposite films

Nanofibrous fillers can lead to composite materials with better mechanical properties than those of the neat polymers. However, their reinforcing effect depends on many factors, including filler morphologies, filler concentration and filler dispersion in matrices and filler adhesion with matrices [1-7,25-32]. The mechanical properties of neat PEO and ChNF/PEO composite films are shown in Fig. 2. Interestingly, the elastic modulus and tensile strength increased significantly with increasing ChNF loading, up to a factor of ~3 times for 20% ChNF compared to neat PEO. It is worth noting that a previous study by Xu et al. on the reinforcing effects of cellulose nanocrystals and cellulose nanofibrils in PEO matrices displayed a maximum at 7% loading of the nano-fibrous fillers [32]. The authors found that the tensile strength and modulus of the prepared composites initially increased when loading fillers up to 7% and then decreased as cellulose content further increased. They further reasoned that the decreases in mechanical properties at higher filler loading resulted from filler agglomeration [32]. In contrast, the ChNFs obtained through a



Fig. 1. Fractured cross section (A) and top-view (C) SEM images of 10% ChNF/PEO composites. Fractured cross section (B) and top-view (D) SEM images of 20% ChNF/PEO composites. Top-view SEM images of dried solvent-washed 10% (E) and 20% (F) ChNF/PEO composites.

high-pressure homogenizer in this work exhibited a more uniform size, less entanglement and smaller bundles and were more well dispersed in the PEO matrix (Fig. 1 and Fig. S1). Herein, the continuous increases in tensile strength and modulus of ChNF/ PEO composites with up to 20% ChNF loading are likely due to ChNFs' high mechanical properties, strong adhesion between PEO and ChNFs (as demonstrated below in FTIR and adhesion results), and good dispersion of ChNFs in the PEO matrix, resulting in efficient stress transfer within the ChNF network structure observed in SEM above. It is possible that beyond 20% ChNF loading filler agglomeration might be observed, leading to a maximum in modulus and strength. However, due to difficulties in drying films at loadings beyond 20% ChNF using the solvent casting method (due to extra water added in the ChNF suspension), we did not examine loading above 20% ChNF.

On the other hand, Fig. 2d shows that strain-at-break of the materials increased and then decreased as ChNF loading increased. Strain hardening was observed for composites comprising 5%, 10% and 15% ChNF, likely due to the alignment of the ChNFs during sample elongation. In contrast, the 20% ChNF composite did not show strain hardening behavior.

3.3. FTIR of ChNF/PEO nanocomposite films

In terms of chemical structures of chitin and PEO, it is expected that hydrogen bonds may form between them since the ether oxygen (C–O–C) in PEO is a hydrogen bond acceptor and there are -OH and -NH hydrogen bond donors in chitin. Infrared spectroscopy is a highly effective method for investigating hydrogen bond interactions in blend composites [33]. As shown in Fig. 3, the characteristic absorption bands for PEO are detected at 1095 and 2878 cm⁻¹, which are attributed to C–O–C stretching and CH₂ stretching, respectively [33,34]. The characteristic peaks of chitin such as the amide band I at 1654 and 1620 cm⁻¹ and the amide band II at 1554 cm⁻¹ are observed [8,9]. All these characteristic peaks from chitin and PEO can be detected in all the composites. With decreasing ChNF loading from 100% to 5%, the amide I and amide II shift to higher frequencies from 1620 to 1628 cm⁻¹and from 1554 to 1562 cm⁻¹, respectively (Fig. 4). This suggests that ChNF-ChNF hydrogen bonds involving the amide nitrogen have been disrupted after addition of PEO by formation of hydrogen bonds between surface-NH groups on ChNF fibers and the ether oxygen of PEO. We note that the h-bonds between O–H ... N (29 kJ/



3.4. Interaction of ChNF with polymer films

An alternative possibility is that ChNF-ChNF h-bonds are broken during fiber dispersion without any new PEO-ChNF hbonds formed, which is difficult to ascertain using ATR-FTIR alone. To provide additional characterization of the nature of ChNF adhesion with PEO, adhesion force measurements were conducted using an AFM colloidal probe method. Fig. 5 shows the morphologies of the ChNF-coated PS particle that was attached to the tipless cantilever. The adsorption of ChNFs on the PS surface was driven by their electrostatic attraction, where the PS particle has a negative charge due to surface sulfate groups and ChNF has positive charge because of protonated $-NH_3^+$ groups. Five kinds of polymer substrates (PE, PS, PVAc, PVOH and PEO) were chosen to examine the effect of surface chemistry on the adhesion forces of ChNFs. The surface roughness, contact angles and calculated surface tension components of these polymers are listed in Tables 1-3. As shown in Table 3, PE and PS are essentially apolar, while PEO, PVAc and PVOH have large Lewis basic components, where lone electron pairs are provided by ether, carbonyl and hydroxyl groups, respectively. These surface tension results are consistent with polarity considerations of the molecular structures.

As shown in Fig. 6, the adhesion forces for bare PS were independent of the polymer surface types. (Fig. S3 shows the typical raw force—distance curves for ChNF-coated PS particles on varied polymer surfaces, which indicates that their interactions are in a short-range (<5 nm).) This is consistent with the expectation that adhesion between PS and the polymer surfaces is governed by VDW forces. Furthermore, according to the Hamaker model, VDW adhesion between a particle and a flat surface depends on the Hamaker constant and a contact radius, which should be approximated well by the Hamaker model [37].

$$F_{\text{Hamaker}} = \frac{AR}{6d^2} \tag{3}$$

Since the values of the Hamaker constant for these five polymers are very close ($\sim 8-9 \times 10^{-20}$ J), the VDW forces are determined largely by the contact radius [38]. Therefore, the similar VDW adhesion forces between bare PS and these polymer surfaces suggest that the small variation in surface roughness of these polymers (Table 1) didn't affect their contact radii.

In contrast, the adhesion forces for ChNF-coated PS were all higher than PS alone, and they varied with different polymer surfaces (Fig. 6). The marked increase in adhesion for ChNF-coated PS on PE and PS, apolar surfaces, is indicative of an increase in contact area for the ChNF-coated PS probes, which is consistent with the added roughness due to the ChNF coating observed in Fig. 5. PE, the most apolar in the series, shows the lowest adhesion force value, while PVAc, PVOH, and PEO with high Lewis basic components possess higher adhesion forces. Typically, the short-range interaction (<5 nm) includes dispersion (nonpolar, VDW force) and non-dispersion force (polar, acid-base interaction). Since the γ^{vW} of these polymer surfaces are not significatly different (Table 3), the VDW forces for ChNF are almost independent of polymer surface

Fig. 2. (a) Representative stress-strain curves, (b) elastic modulus, (c) tensile strength and (d) strain-at-break of neat PEO and ChNF/PEO composites.



Fig. 3. FTIR spectra of each composite films: (a) neat PEO, (b) 5% ChNF/95% PEO, (c) 10% ChNF/90% PEO, (d) 15% ChNF/85% PEO, (e) 20% ChNF/80% PEO, and (f) neat ChNF.



Fig. 4. FTIR spectra of composite films in the 1500–1800 $\rm cm^{-1}$ region: (a) neat PEO, (b) 5% ChNF/95% PEO, (c) 10% ChNF/90% PEO, (d) 15% ChNF/85% PEO, (e) 20% ChNF/80% PEO, and (f) neat ChNF.

Table 1

Surface roughness of the various polymer surfaces.

Surface	PE	PS	PVAc	PVOH	PEO
Ra(nm)	$\begin{array}{c} 4.2 \pm 0.8 \\ 4.3 \pm 0.8 \end{array}$	2.4 ± 0.4	1.5 ± 0.3	1.6 ± 0.4	8.3 ± 2.2
rms (nm)		2.8 ± 0.4	1.7 ± 0.3	1.9 ± 0.4	8.7 ± 2.4

Table	2	

Table 3

Contact angles () of polymer surfaces with three testing liquids.

Substrate	Water	Glycerol	Diiodomethane
PE	105.2 ± 4.0	87.3 ± 2.1	52.8 ± 2.0
PS	101.1 ± 3.0	84.2 ± 2.0	33.6 ± 2.0
PVAc	60.7 ± 2.9	70.7 ± 3.0	37.8 ± 3.0
PVOH	46.2 ± 1.4	44.0 ± 1.3	40.4 ± 1.4
PEO	19.0 ± 4.0	46.8 ± 2.0	33.8 ± 2.5
Chitin	56.7 ± 1.4	46.7 ± 1.4	37.4 ± 2.0

Tuble 5					
Surface tension	components /	(mI/m^2) of	various	polymor	curfacor

	1	,	J	
Surface	γ ^{vW}	γ^+	Υ¯	γ
PE	33	0	0	33.0
PS	43	0.2	0.4	43.2
PVAc	41	0.6	16.7	46.8
PVOH	39	1.1	28.8	50.4
PEO	43	0	64.0	43.0
Chitin	41	1.3	17.1	50.4

types. Therefore, the differences in adhesion forces suggest that Lewis acidic and basic components of the polymer surfaces play an important role in adhesion with ChNF.

Assuming van Oss and Good's Lifshitz—van der Waals acid-base theory for the solid (chitin surface, Ch)-solid (polymer surface, P) interface, the relationship of the adhesion force with the surface energy of the polymers can be expressed as:

$$F_{ad} \propto a \sqrt{\gamma_{ch}^{\nu w} \gamma_P^{\nu w}} + b \sqrt{\gamma_{ch}^+ \gamma_P^-} + c \sqrt{\gamma_{ch}^- \gamma_P^+}$$
(4)

where, F_{ad} is the experimentally determined adhesion force, and *a*, *b* and *c* are coefficients scaling the VDW and acidic-basic contributions, respectively. Since the VDW components of the five polymers (γ_P^{vW}) are similar, Eq. (4) can be simplified to:

$$F_{ad} \propto A + b \sqrt{\gamma_{ch}^+ \gamma_P^-} + c \sqrt{\gamma_{ch}^- \gamma_P^+} \tag{5}$$

where *A* is a constant representing VDW-driven adhesion. We fitted the adhesion force data to Eq. (5), which is shown as a plane in Fig. 7. Fitting all five polymers led to a correlation coefficient of r^2 ~0.88, suggesting that the differences of total adhesion forces on



Fig. 5. (A) SEM image of an AFM probe of ChNF-coated PS particle after all AFM force measurements; (B) Enlarged SEM image of surface morphology of ChNF-coated PS particle.



Fig. 6. Adhesion forces for ChNF-coated and bare PS particles on various polymer surfaces.



Fig. 7. Fitting of the planar model of Eq. (4) to adhesion force data for ChNF-coated PS colloidal probes with five substrates of varying polarity.

varied surfaces can be explained by acid-base (h-bonding interactions) of the polymer surfaces. Further, the relative contributions of acidic and basic components are not too different, b/c = 1.46. Carbonyl, hydroxyl and ether oxygens in the polymers that possess them act as the major electron donor components and are able to form hydrogen bonds with -OH, -NH and $-NH_2$ groups on the chitin structures. Since PEO has the largest γ^- value, indicative of its electron donors (hydrogen bond acceptors), and because chitin has protons that can serve as hydrogen bond donors, such as-OH, -NH- and $-NH_2$, we conclude that the acid-base interaction between PEO and chitin are hydrogen bonds. This is consistent with FTIR data presented above.

Table 4

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Sample	T _m (°C)	ΔH (J/g)	X _c (%)
Neat PEO	67.3	177.0	86.3
5% Chitin/PEO	65.8	165.5	85.0
10% Chitin/PEO	64.0	152.3	82.6
15% Chitin/PEO	62.7	137.4	78.9
20% Chitin/PEO	62.0	122.3	74.6

3.5. DSC analysis

The melting temperature (T_m) , enthalpy of fusion and crystallinity (X_c) of neat PEO and ChNF/PEO composite films were measured using DSC. The degree of crystallinity of these samples was calculated according to Eq. (6) [39].

$$X_c = \frac{\Delta H_i}{f_i \Delta H_i^m} \times 100\% \tag{6}$$

where, ΔH_i is the enthalpy of fusion of the prepared PEO samples, obtained from DSC measurements, f_i is the mass fraction of PEO in the composite, and ΔH_i^m is the enthalpy of fusion of 100% crystalline PEO, which is 205 J/g [39]. The neat PEO has a melting temperature of 67.3 °C and crystallinity of 86.3% (Table 4), and the crystallinity and melting temperature of PEO decreased with increasing ChNF loading. We reason that the dispersion of ChNF in the PEO matrix and strong interactions between ChNF and PEO hindered chain diffusion and folding during PEO crystallization, resulting in the low crystallinity for composite samples. The neat PEO has a T_g of -56.2 °C while the T_g of 5%, 10% and 15% ChNF/PEO composites are -49.2, -48.7 and -48.4 °C, respectively. The increase in glass transition temperature and decrease in crystallinity with ChNF content for the composites is consistent with the strong adhesion between ChNF and PEO that likely restricts PEO chain mobility.

4. Conclusions

In this study, ChNF/PEO nanocomposites were successfully fabricated by an aqueous solution casting method and the structure-property relationships of the nanocomposites were investigated. ChNFs were dispersed well and formed interconnected network structures in the PEO matrix. Compared to neat PEO, the tensile strength and elastic modulus of the nanocomposites increased ~3 times at 20% ChNF loading. In addition to ChNFs' high mechanical properties, the strong interactions between ChNF and PEO, and the ChNF network structure played important roles in efficient stress transfer from matrix to fiber and from fiber to fiber. The ATR-FTIR and AFM colloidal probe adhesion measurements support the conclusion that ChNF has strong hbond and VDW-driven adhesion with itself and with PEO.

The crystallinities of PEO in composites are lower than that of neat PEO, which may be attributed to dispersion of ChNF in the PEO matrix and strong interactions between ChNF and PEO that restrict the chain mobility during PEO crystallization. Processing ChNFs in suspensions with slight acidity and water-soluble polymers appears to support the formation of highly interconnected networks that makes ChNF-polymer composites excellent candidates for reinforced, light-weight, renewable materials.

Author contributions

The manuscript was written through contributions of all authors. All authors have given approval to the final version of the manuscript.

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Appendix A. Supplementary data

Supplementary data related to this article can be found at http://dx.doi.org/10.1016/j.polymer.2016.01.017.

References

- T. Chatterjee, K. Yurekli, V.G. Hadjiev, R. Krishnamoorti, Single-walled carbon nanotube dispersions in poly(ethylene oxide), Adv. Funct. Mater. 15 (2005) 1832–1838.
- [2] L.A. Goettler, K.Y. Lee, H. Thakkar, Layered silicate reinforced polymer nanocomposites: development and applications, Polym. Rev. 47 (2007) 291–317.
- [3] T. Chatterjee, C.A. Mitchell, V.G. Hadjiev, R. Krishnamoorti, Hierarchical polymer-nanotube composites, Adv. Mater. 19 (2007) 3850.
- [4] S.Y. Fu, X.Q. Feng, B. Lauke, Y.W. Mai, Effects of particle size, particle/matrix interface adhesion and particle loading on mechanical properties of particulate-polymer composites, Compos. Part B-Engineering 39 (2008) 933–961.
- [5] B. Chen, J.R.G. Evans, H.C. Greenwell, P. Boulet, P.V. Coveney, A.A. Bowden, A. Whiting, A critical appraisal of polymer-clay nanocomposites, Chem. Soc. Rev. 37 (2008) 568–594.
- [6] S. Bredeau, S. Peeterbroeck, D. Bonduel, M. Alexandre, P. Dubois, From carbon nanotube coatings to high-performance polymer nanocomposites, Polym. Int. 57 (2008) 547–553.
- [7] D. Klemm, F. Kramer, S. Moritz, T. Lindstrom, M. Ankerfors, D. Gray, A. Dorris, Nanocelluloses: a new family of nature-based materials, Angew. Chemie-International Ed. 50 (2011) 5438–5466.
- [8] M. Rinaudo, Chitin and chitosan: properties and applications, Prog. Polym. Sci. 31 (2006) 603–632.
- [9] C.K.S. Pillai, W. Paul, C.P. Sharma, Chitin and chitosan polymers: chemistry, solubility and fiber formation, Prog. Polym. Sci. 34 (2009) 641–678.
- [10] J.-B. Zeng, Y.-S. He, S.-L. Li, Y.-Z. Wang, Chitin whiskers: an overview, Biomacromolecules 13 (2012) 1–11.
- [11] J. Wu, K. Zhang, N. Girouard, J.C. Meredith, Facile route to produce chitin nanofibers as precursors for flexible and transparent gas barrier materials, Biomacromolecules 15 (2014) 4614–4620.
- [12] J. Wu, J.C. Meredith, Assembly of chitin nanofibers into porous biomimetic structures via freeze drying, Acs Macro Lett. 3 (2014) 185–190.
- [13] M. Trollsås, J.L. Hedrick, Dendrimer-like star polymers, J. Am. Chem. Soc. 120 (1998) 4644–4651.
- [14] A.C. Albertsson, I.K. Varma, Recent developments in ring opening polymerization of lactones for biomedical applications, Biomacromolecules 4 (2003) 1466–1486.
- [15] K. Gopalan Nair, A. Dufresne, Crab shell chitin whisker reinforced natural rubber nanocomposites. 1. processing and swelling behavior, Biomacromolecules 4 (2003) 657–665.
- [16] S. Ifuku, M. Nogi, K. Abe, M. Yoshioka, M. Morimoto, H. Saimoto, H. Yano, Preparation of chitin nanofibers with a uniform width as alpha-chitin from crab shells, Biomacromolecules 10 (2009) 1584–1588.
- [17] J.C. Meredith, A. Karim, E.J. Amis, High-throughput measurement of polymer

blend phase behavior, Macromolecules 33 (2000) 5760-5762.

- [18] B.J.R. Thio, J.H. Lee, J.C. Meredith, Characterization of ragweed pollen adhesion to polyamides and polystyrene using atomic force microscopy, Environ. Sci. Technol. 43 (2009) 4308–4313.
- [19] J.L. Hutter, J. Bechhoefer, Calibration of atomic-force microscope tips, Rev. Sci. Instrum. 64 (1993) 1868–1873.
- [20] R.J. Good, C.J. van Oss, Modern Approach of Wettability: Theory and Applications, Plenum Press, New York, 1991.
- [21] H.J. Busscher, J. Arends, Determination of the surface forces gamma-s-d and gamma-s-p from contact-angle measurements on polymers and dental enamel, J. Colloid Interface Sci. 81 (1981) 75–79.
- [22] K.X. Ma, T.S. Chung, R.J. Good, Surface energy of thermotropic liquid crystalline polyesters and polyesteramide, J. Polym. Sci. Part B-Polymer Phys. 36 (1998).
- [23] J.L. Sormana, J.C. Meredith, High-throughput discovery of structuremechanical property relationships for segmented poly(urethane-urea)s, Macromolecules 37 (2004) 2186–2195.
- [24] J.L. Sormana, S. Chattopadhyay, J.C. Meredith, High-throughput mechanical characterization of free-standing polymer films, Rev. Sci. Instrum. 76 (2005).
 [25] M. Samir, F. Alloin, M. Paillet, A. Dufresne, Tangling effect in fibrillated cel-
- [25] M. Samir, F. Alloin, M. Paillet, A. Dufresne, Tangling effect in fibrillated cellulose reinforced nanocomposites, Macromolecules 37 (2004) 4313–4316.
- [26] M.O. Seydibeyoglu, K. Oksman, Novel nanocomposites based on polyurethane and micro fibrillated cellulose, Compos. Sci. Technol. 68 (2008) 908–914.
- [27] A. Iwatake, M. Nogi, H. Yano, Cellulose nanofiber-reinforced polylactic acid, Compos. Sci. Technol. 68 (2008) 2103–2106.
- [28] F. Dalmas, J.-Y. Cavaille, C. Gauthier, L. Chazeau, R. Dendievel, Viscoelastic behavior and electrical properties of flexible nanofiber filled polymer nanocomposites. Influence of processing conditions, Compos. Sci. Technol. 67 (2007) 829–839.
- [29] Q. Cheng, S. Wang, T.G. Rials, Poly(vinyl alcohol) nanocomposites reinforced with cellulose fibrils isolated by high intensity ultrasonication, Compos. Part a-Applied Sci. Manuf. 40 (2009) 218–224.
- [30] G. Chinga-Carrasco, Cellulose fibres, nanofibrils and microfibrils: the morphological sequence of MFC components from a plant physiology and fibre technology point of view, Nanoscale Res. Lett. 6 (2011).
- [31] K.-Y. Lee, T. Tammelin, K. Schulfter, H. Kiiskinen, J. Samela, A. Bismarck, High performance cellulose nanocomposites: comparing the reinforcing ability of bacterial cellulose and nanofibrillated cellulose, Acs Appl. Mater. Interfaces 4 (2012) 4078–4086.
- [32] X. Xu, F. Liu, L. Jiang, J.Y. Zhu, D. Haagenson, D.P. Wiesenborn, Cellulose nanocrystals vs. cellulose nanofibrils: a comparative study on their microstructures and effects as polymer reinforcing agents, Acs Appl. Mater. Interfaces 5 (2013) 2999–3009.
- [33] J. Jin, P. Hassanzadeh, G. Perotto, W. Sun, M.A. Brenckle, D. Kaplan, F.G. Omenetto, M. Rolandi, A biomimetic composite from solution selfassembly of chitin nanofibers in a silk fibroin matrix, Adv. Mater. 25 (2013) 4482–4487.
- [34] E.E. Brown, M.-P.G. Laborie, Bloengineering bacterial cellulose/poly(ethylene oxide) nanocomposites, Biomacromolecules 8 (2007) 3074–3081.
- [35] J. Emsley, Very strong hydrogen-bonding, Chem. Soc. Rev. 9 (1980) 91–124.
 [36] J.W. Larson, T.B. McMahon, Gas-phase bihalide and pseudobihalide ions. An ion cyclotron resonance determination of hydrogen bond energies in XHY-species (X, Y = F, Cl, Br, CN), Inorg. Chem. 23 (1984) 2029–2033.
- [37] J. Israelachvili, Intermolecular and Surface Forces, Acadamic Press, London, 1992.
- [38] H. Lin, I. Gomez, J.C. Meredith, Pollenkitt wetting mechanism enables speciesspecific tunable pollen adhesion, Langmuir 29 (2013) 3012–3023.
- [39] I.T. Kim, J.H. Lee, M.L. Shofner, K. Jacob, R. Tannenbaum, Crystallization kinetics and anisotropic properties of polyethylene oxide/magnetic carbon nanotubes composite films, Polymer 53 (2012) 2402–2411.